



# Electrical Insulation Breakdown Strength and Thermal Conductivity of Different Blended Nanocomposites of New Epoxy Resins

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## Abstract

This research studies the development and synthesis of blended nanocomposites filled with Titanium dioxide ( $\text{TiO}_2$ ). Blended nanocomposites based on unsaturated polyester resin (UPR) and epoxy resins were synthesized by reactive blending. The optimum quantity from nano partical of titanium dioxide was selected and different weight proportions 1%, 3%, 5%, and 7% ratios of new epoxy are blended with UPR resin. The dielectric breakdown strength and thermal conductivity properties of the blended nanocomposites were compared with those of the basis material (UPR and 3%  $\text{TiO}_2$ ).The results show good compatibility epoxy resins with the UPR resin on blending, dielectric breakdown strength values are higher while thermal conductivity values of blends nanocomposites are significantly lower compared to that of the(UPR and 3%  $\text{TiO}_2$ ), semi-interpenetrating UPR/Epoxy blends (semi-IPNs) for one type of new epoxy [P<sub>2</sub>]was prepared and noticed the blend nanocomposites show higher dielectric breakdown strength than the semi- IPNs (UPR/Epoxy) at low loading of new epoxies but the thermal conductivity is a higher than the semi- IPNs UPR/Epoxy at all loading. Thermogravimetric analysis (TGA) was employed to study the thermal properties of the blended nanocomposites.

**Key word:** blened nanocomposite: unsaturated polyester resin: epoxy resin: dielectric breakdown strength.

## Introduction

With the rapid development of the electronic information industry, better properties are required for substrate and packaging materials such as low coefficient of thermal expansion (CTE), low dielectric constant, high electric insulation, and high thermal stability. Therefore, many studies have been focused on developing new materials with superior strength and attributes[1].

In the nano studies with notable researches advances that revealed new physical phenomena and improved material properties in the nano-sized since ,the introduction of nanofillers demonstrate several advantages in their properties when compared with the similar properties obtained for epoxy systems with micrometer sized fillers [2-5] polymer nanocomposites have attracted considerable attention from both fundamental research and application points of view, because it exhibited much better mechanical, thermal, and multifunctional properties in comparison with the polymer matrices and their conventional microcomposite and macrocomposite counterparts.[1].

Epoxy resins are well-known materials in the field of insulation systems for heavy electric equipment such as mold-type transformers, potential transformers (PT), current transformers (CT), and metering out-fit (MOF) because the epoxy resin provides essential electrical, thermal, and mechanical properties. In the last two decades, rapid development of epoxy-based composites in electric applications has been achieved to give the epoxy resins much higher electrical performance with lower cost [6,7]. Unsaturated polyester resins (UPR) are comparatively hard and brittle materials and one of the important thermosetting materials used for the manufacture of glass-reinforced plastics and polymeric composites. These resins have wide spread use which is due to their relatively low cost, comfortable of processing, high wetting properties with reinforcements[8] .There are many reports that the technique of polymer blending is a useful method to obtain a new insulating material[9].

For the design of these insulating materials the most important parameter is dielectric voltage breakdown strength. This is used to measure the failure strength of the insulation against the applied electric field. It is to be noted that, when electrical breakdown occurs due to high applied voltage it results in a fracture due to breaking of insulation barrier as well generation of electrical sparks. Li et al[10] observed that hybrid nano/micro  $\text{Al}_2\text{O}_3$  epoxy composite exhibits higher partial discharge resistance as compared to micro  $\text{Al}_2\text{O}_3$ /epoxy composite. In addition, epoxy/nano- $\text{TiO}_2$  composite show improved alternating current AC voltage endurance, and dielectric strengths compared to its micro size  $\text{TiO}_2$  filled epoxy composite[11]

With respect to the electrical breakdown characteristics in polymer nanocomposites, several reports are available on different polymeric systems. In epoxy nanocomposites filled with  $\text{TiO}_2$  fillers, the voltage endurance (AC), short-term direct current and alternating (DC , AC) dielectric strengths and impulse breakdown strengths are found to be higher as compared to microcomposites [5]

Thermal conductivity of polymers is an important thermal property for both polymer applications and processing. Polymers typically have intrinsic thermal conductivity much lower than those for metals or ceramic materials, and therefore are good thermal insulators. In other applications which require higher thermal conductivity, such as in electronic packaging and encapsulations, satellite devices, and in areas where good heat dissipation, low thermal expansion and light weight are needed, polymers reinforced with fillers, organic or inorganic, are becoming more and more common in producing advanced polymer composites for these applications[12]. In a solid material, there are two main mechanisms of heat conduction: through elastic waves, which are called phonons, and through free electrons. Polymer materials generally do not have freely moving electrons. So,

heat transfer has effected only via elastic waves. The electron conductivity is dominant in metals and absent in insulators [13].

Thermal conductivities of polymer materials depend on many factors, such as chemical constituents, strength of bonding, structure type, molecular weight of side groups, molecular density distribution, type and strength of defects or structural faults, size of intermediate range order, processing conditions and temperature, etc [14]. Commonly used polymer materials are materials of low thermal conductivity. The typical range of polymers is from 0.17 to 0.35 W/mK [15]. Epoxy resin is one of the common materials that is used for electrical insulation. In spite of the excellent performance of epoxy, its relatively low thermal conductivity cannot satisfy the increased demands of new electronic devices. Improved thermal conductivity in polymers may be achieved either by changing the molecular orientation, by the addition of conductive fillers [16] or by synthesizing the polymer materials with enhanced thermal conductivity [17].

In this study, an epoxy/ UPR /TiO<sub>2</sub> composites were prepared, with particle sizes of 10-15nm; an electrical insulation breakdown test and thermal conductivity were then carried out.

## 2. Experimental

### Materials

All the raw materials were supplied from Merck, GCC and Aldrich Chemicals Co. and used as received.

### Testing

The FTIR spectrum of UPR/TiO<sub>2</sub> and blended nanocomposites were taken using bromide discs on a Shimadzo (IR prestige-21) FTIR spectrophotometer. <sup>1</sup>H NMR spectra were carried out by company: Bruker, model: ultra-shield 300MHz origin: Switzerland, and Bruker model: ER-av-400MHz, origin: Switzerland are reported in ppm (δ), DMSO was used as solvents. The dielectric voltage breakdown strength and thermal conductivity testing were taken for UPR/TiO<sub>2</sub> and blended nanocomposites. The dielectric breakdown strength properties were tested using the device (Rang HV-50Hz 300 KV). The time rate to increase voltages in electrical breakdown (0.5KeV/ s) and thermal conductivity properties was tested by using A Lee's disc instrument manufactured by the Griffen and George Company, England.

## Methods

### Preparation of monomers [M<sub>1</sub>-M<sub>10</sub>]

The monomer; Bis-[4,4'-hydroxybenzylideneamino]phenol [M<sub>1</sub>], quinoxaline-2,3-diol [M<sub>2</sub>], [2,5-di-(p-hydroxyphenyl)-1,3,4-thiadiazole] [M<sub>3</sub>], 4,4'-diphenylenebis[(azo)-2,4-dihydroxyphenyl] [M<sub>4</sub>], 4-(4'-hydroxybenzylideneamino)phenol [M<sub>5</sub>], 4,4'-diphenylenebis[(azo)phenyl] [M<sub>6</sub>] were prepared according to reference [18], 2-amino-4-(4-aminophenyl)-1,3-thiazole [M<sub>7</sub>] and 2-amino-4-(4-hydroxyphenyl)-1,3-thiazole [M<sub>8</sub>] were prepared according to reference [19], methylene-bis-(2,4-dihydroxyphenyl) [M<sub>9</sub>] was prepared according to the reference [20], and the monomer 1,4-bis(5,5'-2-amino-1,3,4-thiadiazol)phenol [M<sub>10</sub>] was prepared according to the reference [21].

### Preparation of polymers [P<sub>1</sub>-P<sub>10</sub>]

A suitable monomer [M<sub>1</sub>-M<sub>10</sub>] (0.01 mol) was dissolved in 10 % aq. NaOH solution (0.0188 mol) in a three neck round bottom flask which is balanced in an oil bath set at 50°C. A homogeneous solution was obtained after vigorous stirring under reflux followed by



add methyl ethyl ketone peroxide 2% to the mixture and mixed mechanical stirrer for 5 min., its found that 3% is optimum quantity. Table 3 illustrated the results of dielectric breakdown and thermal conductivity on respectively for UPR/TiO<sub>2</sub>.

### Preparation of polymer blend and composite

Unsaturated poly ester, epoxy resin in varying amounts (1,3,5,7%) and optimum quantity from titanium dioxide (TiO<sub>2</sub>) (3%) were mixed together in a suitable beaker, and a mixture was placed in a high intensity ultrasonic bath for 2 hrs at ambient temperature conditions, used ice bath to avoid temperature rise during the sonication process.

Then curing agent methyl ethyl ketone peroxide (2%) part by weight was added to mixture, the mixture was stirred well with mechanical stirring to give a homogeneous mixture, the mixture poured into mold of iron with dimension (15×5×0.4) cm and left overnight. The first curing was done at room temperature followed by a second curing step at 120° C for 2 hrs. When the solidification process is finished the sample was cut down into standard dimensions.

## 3. Results & discussion

### Spectroscopic identification

Polycondensation was successfully conducted between epichlorohydrin and M<sub>1</sub>,M<sub>3</sub>,M<sub>4</sub>,M<sub>5</sub>,M<sub>6</sub>,M<sub>7</sub>,M<sub>8</sub>,M<sub>9</sub> and M<sub>10</sub> using aq. NaOH incentive as shown in Scheme 1. The pure polymer and blended nanocomposite after post curing were studied by FTIR spectrum. The FTIR spectra of the purified epoxy prepolymer of polymer [P1-P10] showed the characteristic C-O band in oxirane ring and ether linkages formed which can be seen in Table 4 presents the principal FTIR stretching vibrations for the epoxy resins. Comparing the FTIR spectrum of UPR/TiO<sub>2</sub>, blended nanocomposites [B1] and polymer P<sub>1</sub> can be seen in Figure 1 the FTIR of blend polymer [B1] showed the appearance of good peak for C=O stretching band at 1722 cm<sup>-1</sup> besides to other characteristic bands of polymer [P1]. The <sup>1</sup>HMNR spectrum (in DMSO as a solvent) for polymer P<sub>2</sub>, showed the following signals: signals in the region δ(7.23-7.60) ppm for aromatic protons and OH proton. Many signals in the range δ (3.91-5.35) ppm for aliphatic protons of CH<sub>2</sub> methylene groups. the <sup>1</sup>HMNR spectrum (in DMSO as a solvent) for P<sub>3</sub> showed: a singlet signal at δ 8.87 ppm for proton of OH group, double of doublet signals at δ (7.32-8.06) ppm that could be attributed to aromatic protons and a signal at δ 5.76 ppm for one proton of CH group. Another signal at δ (4.312-4.44) ppm due to four protons of 2CH<sub>2</sub>O groups. The <sup>1</sup>HMNR spectrum (in DMSO as a solvent) for polymer P<sub>5</sub>, showed the following signals: a singlet signal at δ 9.96 ppm for one proton of OH, a singlet signal at δ 8.56 ppm that could be attributed to proton of imine group (CH=N). Many signals in the region δ(6.59-7.83) ppm are due to aromatic protons. Also, multiplet signal between δ (4.70-5.59) ppm for protons of CH<sub>2</sub>CH in oxirane ring and CH-OH group. while the protons of (2OCH<sub>2</sub>) group appeared in region δ (3.70-4.20) ppm, the <sup>1</sup>HNMR can be seen in Figure (2).

### Dielectric breakdown properties

Dielectric breakdown properties of the composites are mostly affected by the insulating structures, defects and impurities, such as the external factors form, type and the nature of the polar used and outer surface and measurement conditions such as the pressure, temperature, moisture, frequency the source, the time period in the application of voltages, the type and ratio of reinforced used in it. Dielectric breakdown strength values of blends nanocomposites with different weight percentage are significantly higher compared to that of the UPR/TiO<sub>2</sub>. Figure 2 shows that the strength decreases with further increase in weight

percentages of epoxy in some structure. Found where the chain conjugation was interrupted by aliphatic moiety, which led to increase flexibility due to a large volume and increase the conductivity and that led to decrease dielectric breakdown, On the other hand the conductivity was decreased where the chain was interrupted by long aliphatic group which weakened the conjugation in the main chain, so the flexibility effect on conductivity is dominant and dielectric breakdown. Illustrated the results of dielectric breakdown tests of the blended nanocomposite at different weight percentages of epoxy resins, at room temperature were shown in Figure 3 and Table 5.

### **Thermal conductivity properties**

The blend nanocomposites show higher thermal conductivity than the same-IPNs UPR/Epoxy for P<sub>2</sub>, the results showed that the thermal conductivity increases with presence of nanoparticles. When comparing the thermal conductivity for UPR/TiO<sub>2</sub>, blended nanocomposites the results showed that the thermal conductivity decreases with the increase of wt% of epoxy resin, the thermal conductivity of TiO<sub>2</sub>/ UPR/Epoxy nanocomposites attains an optimum value of 0.307933 W/m.K for B<sub>2</sub> at loading 1% wt Epoxy. But when increase %wt of Epoxy with existence percentage a fixed of the TiO<sub>2</sub> led B<sub>2</sub> show minimum value of thermal conductivity. The high density of functional end groups thermosetting hyperbranched epoxy resin is conducive to well dispersion of nanoparticles and improve the compatibilities and interaction between the particles and matrix, thus compromise the comprehensive properties of the thermally conductive. Illustrated the results of thermal conductivity tests of the composite at different weight percentages of epoxy resins, at room temperature were shown in Figure (4) and Table (6).

### **Thermal studies**

TGA analyses for the blended nanocomposites after curing are shown in Figure (5), the blended nanocomposites has thermal stability as shown in Table (7). Illustrated the onset temperature(°C), temperature of maximum (°C) and Temperature of half loss (°C) .

### **Conclusion**

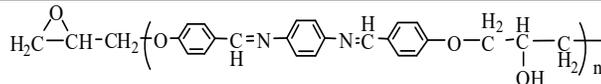
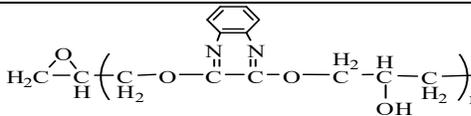
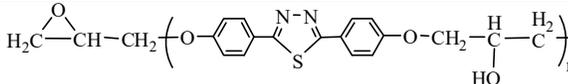
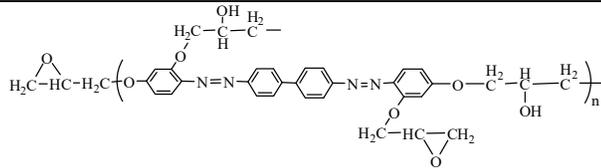
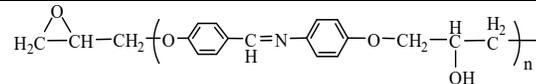
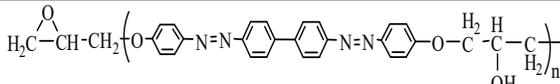
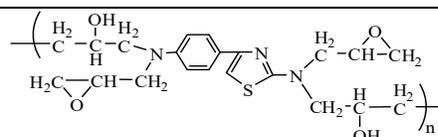
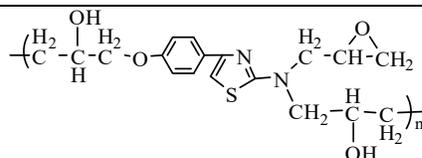
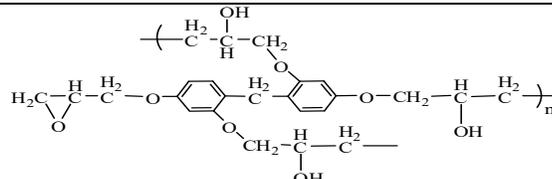
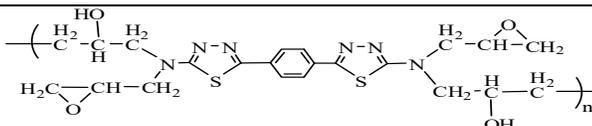
Epoxy prepolymer was successfully prepared, epoxy resins are highly miscible with UPR. Dielectric breakdown property for blended nanocomposites show maximum improvement at about 3% by wt epoxy concentration, for B<sub>9</sub> was 13.57KV/mm. Thermal conductivity lower with the increase of the percentage of epoxy for all blended nanocomposites. The thermal conductivity was increased from K=0.2205 W/mK for S-INPs (UPR/Epoxy P<sub>2</sub>) to 0.255970 by for the B<sub>2</sub> with 3 wt% of epoxy resin. High electrical insulation and thermal conductivity will make TiO<sub>2</sub>/UPR/epoxy nanocomposites promising in the electrical package field. In blended nanocomposites show substantial improvement in thermal stability.

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**Table (1): Summary of compound structure, melting point**

symbol of polymer	Structure of polymer	M.P.
P <sub>1</sub>		>300
P <sub>2</sub>		250
P <sub>3</sub>		>300
P <sub>4</sub>		>300
P <sub>5</sub>		128
P <sub>6</sub>		>300
P <sub>7</sub>		>300
P <sub>8</sub>		>300
P <sub>9</sub>		>300
P <sub>10</sub>		>300

**Table (2): Dielectric breakdown and thermal conductivity properties of S-IPNs UPR with (1, 3,5,7) wt% epoxy resin [P<sub>2</sub>].**

Property	UPR/(1%)wt Epoxy	UPR/(3%)wt Epoxy	UPR/(5%)wt Epoxy	UPR/(7%)wt Epoxy
Dielectric breakdown	9.71	9.91	10.56	11.97
Thermal conductivity	0.235	0.2205	0.2192	0.2102

**Table (3): Dielectric breakdown and Thermal conductivity of properties of UPR+ (1,3,5,7)%TiO<sub>2</sub> modified**

Property	UPR/TiO <sub>2</sub> (1%)	UPR/ TiO <sub>2</sub> (3%)	UPR/TiO <sub>2</sub> (5%)	UPR/TiO <sub>2</sub> (7%)
Dielectric breakdown	5.87	9.24	8.27	7.28
Thermal conductivity	0.29287	0.38438	0.29585	0.2860

**Table (4): Summary of identification of infrared bands for epoxy resins[ P<sub>1</sub>-P<sub>10</sub>]**

Polymer No.	OH cm <sup>-1</sup>	C-Hcm <sup>-1</sup> aromatic	C-H cm <sup>-1</sup> aliphatic	C=N cm <sup>-1</sup>	C=C cm <sup>-1</sup>	C-O-C cm <sup>-1</sup>	C-O ring cm <sup>-1</sup>	others
P <sub>1</sub>	3369.64	3060	2927.94	1676.14	1512.19	1217	914.26	—
P <sub>2</sub>	3419.79	3070	2935.66	1649.14	1595.13	1269.16	918.12	—
P <sub>3</sub>	3400.50	3060	2931.80	1602.85	1504.48	1238.30	952.84	—
P <sub>4</sub>	3400.50	3060	2935.66	—	1597.06	1246.02	914.26	N=N1460.11
P <sub>5</sub>	3388.93	3076.46	2931.80	1678.07	1575.84	1240	914.26	—
P <sub>6</sub>	3409.33	3054.41	2930.96	—	1495.86	1234.18	943.23	N=N1460.18
P <sub>7</sub>	3325.28	3030	2918.30	1606.70	1515.5	1257.59	929.69	—
P <sub>8</sub>	3315.63	3010	2924.09	1604.77	1533.34	1240.23	939.33	—
P <sub>9</sub>	3394.72	3000	2939.52	—	1510	1246.02	941.61	—
P <sub>10</sub>	3377.36	3001	2945.30	1608.63	1552.70	1265.3	939.33	—

**Table (5): Summary of dielectric breakdown properties of blended nanocomposites (B<sub>1</sub>-B<sub>10</sub>)with (1,3,5,7) wt% epoxy resins in the present 3%TiO<sub>2</sub>.**

Compound No.	Dielectric breakdown Strength KV/mm			
	UPR+1%epoxy	UPR+3%epoxy	UPR+5%epoxy	UPR+7%epoxy
B <sub>1</sub>	10.24	11.07	10.27	9.6
B <sub>2</sub>	10.22	11.97	9.87	9.8
B <sub>3</sub>	12.9	11.17	10.9	10.5
B <sub>4</sub>	12.18	12.9	12.3	11.78
B <sub>5</sub>	11.2	12.8	12.07	11.78
B <sub>6</sub>	12.15	11.42	10.97	11.87
B <sub>7</sub>	12.18	12.57	12.97	11.96
B <sub>8</sub>	11.5	12.45	12.01	11.32
B <sub>9</sub>	12.48	13.67	13.64	11.7
B <sub>10</sub>	10.16	10.61	11.74	10.8

**Table (6): Summary of thermal conductivity properties of blended nanocomposites [B<sub>1</sub>-B<sub>10</sub>] with (1,3,5,7) wt% epoxy resins in the present 3% TiO<sub>2</sub>.**

Compound No.	Thermal conductivity Strength W/mK			
	UPR+1%epoxy	UPR+3%epoxy	UPR+5%epoxy	UPR+7%epoxy
B <sub>1</sub>	0.414000	0.300665	0.239722	0.274821
B <sub>2</sub>	0.307933	0.255970	0.234000	0.232596
B <sub>3</sub>	0.309000	0.257000	0.244063	0.239500
B <sub>4</sub>	0.300007	0.327208	0.321062	0.272081
B <sub>5</sub>	0.32162	0.301871	0.275231	0.231677
B <sub>6</sub>	0.289663	0.271310	0.277302	0.225242
B <sub>7</sub>	0.248258	0.234637	0.231171	0.215556
B <sub>8</sub>	0.295200	0.280180	0.273146	0.268891
B <sub>9</sub>	0.243371	0.267000	0.23783	0.27851
B <sub>10</sub>	0.158733	0.196705	0.187540	0.18324

**Table (7): Thermal properties-TGA blended nanocomposites in the present 3% TiO<sub>2</sub>.**

Blend NO.	Onset temperature (°C)	Temperature of maximum (°C)	Temperature of half loss (°C)	Temperature of melt(°C)
UPR/TiO <sub>2</sub>	281.1	409.1	389.2	556.7
B <sub>1</sub>	268.9	404	386.5	552
B <sub>2</sub>	263.5	379.7	405.3	540.5
B <sub>3</sub>	197	405.8	371.6	537.4
B <sub>4</sub>	192	406.2	365	547.3
B <sub>8</sub>	264.9	395.6	372	552.7

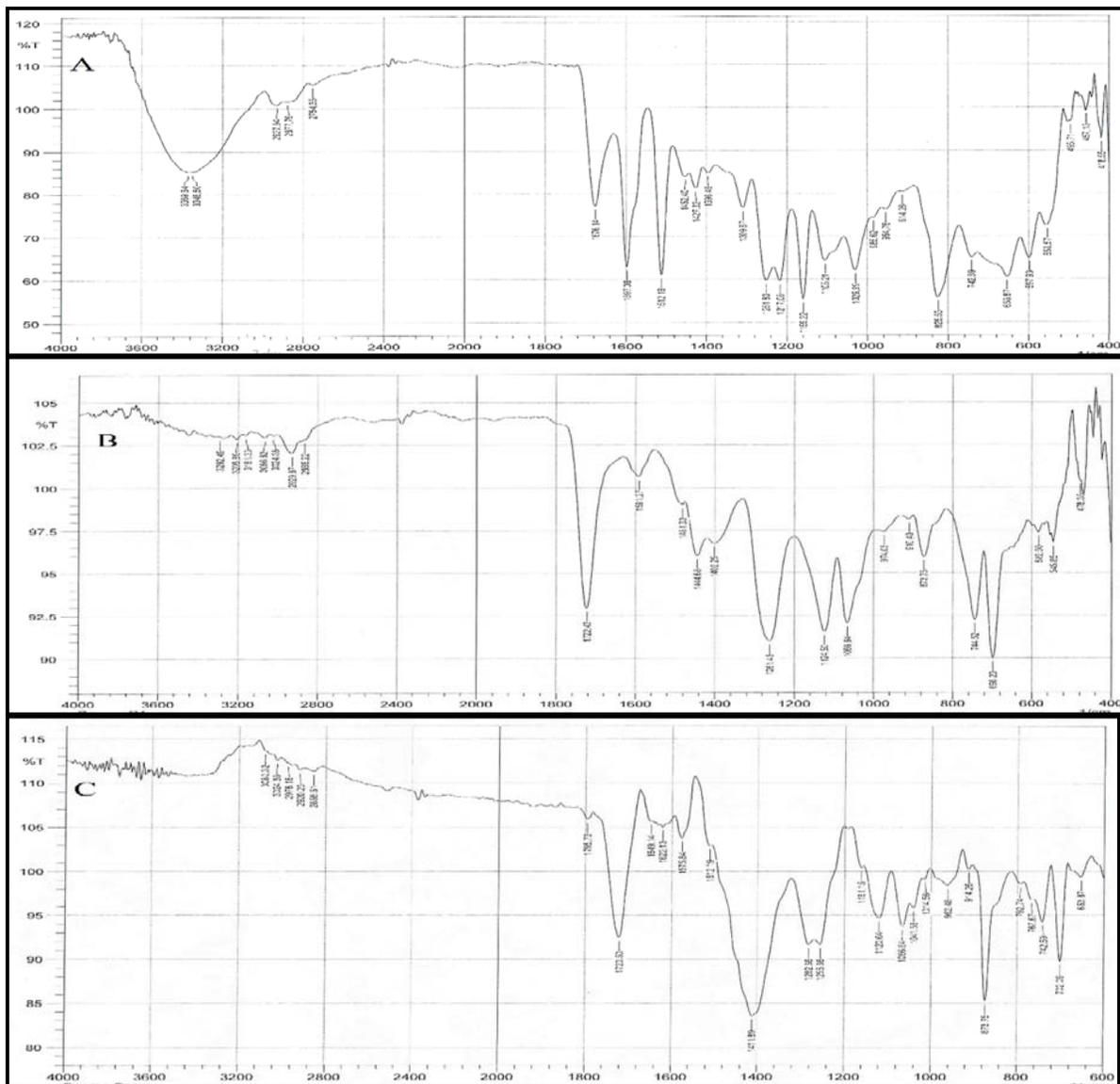


Figure (1) A: The FTIR –spectrum of [ P<sub>1</sub> ], B: The FTIR –spectrum of blended nanocomposite [ B<sub>1</sub>], C: The FTIR –spectrum of UPR/TiO<sub>2</sub>.

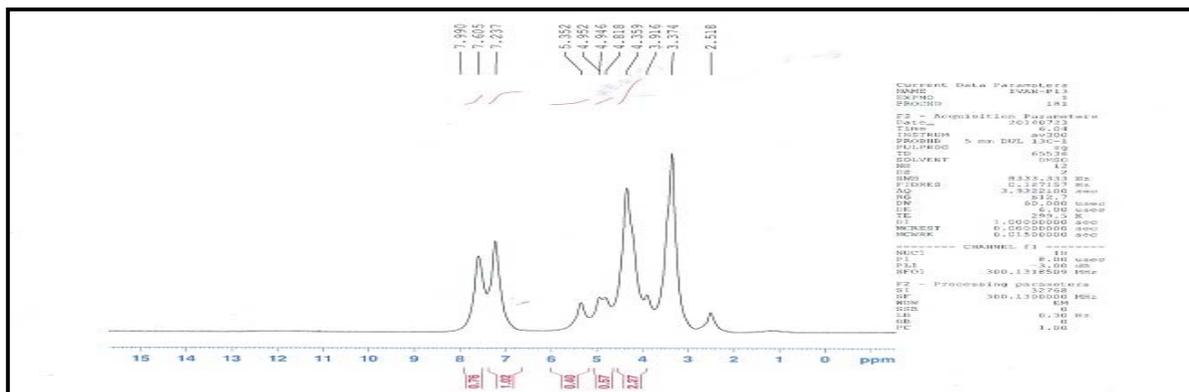


Figure (2) A: The <sup>1</sup>H NMR –spectrum of [ P<sub>2</sub> ]

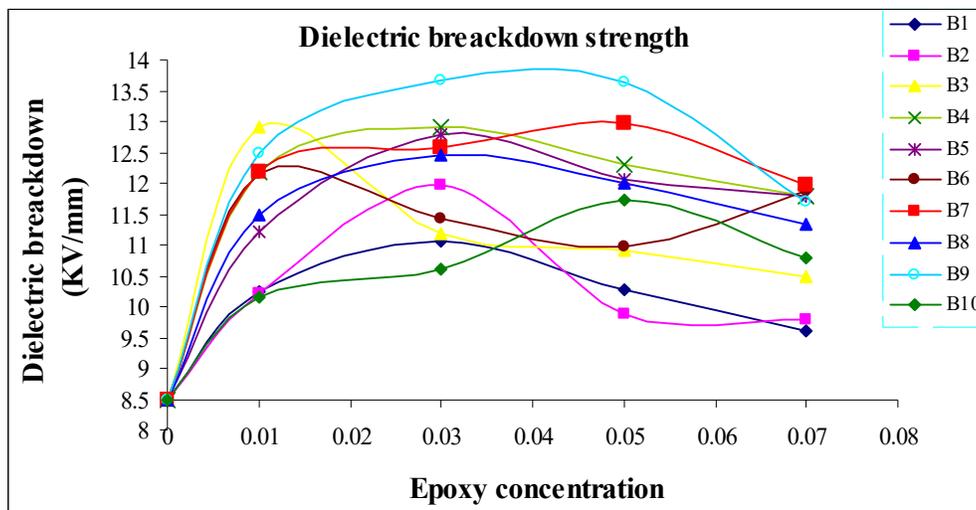


Figure (3): Dielectric breakdown properties strength of blended nanocomposites versus epoxy concentration

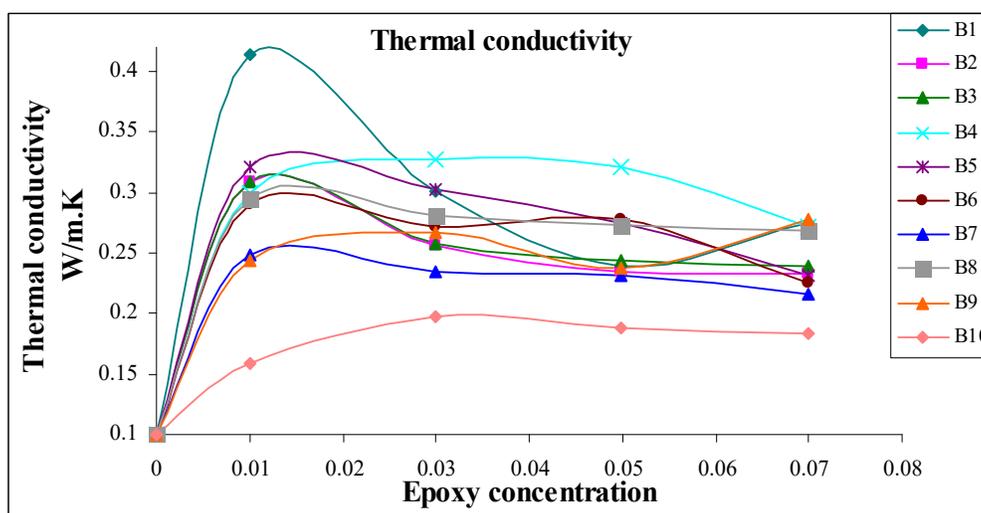
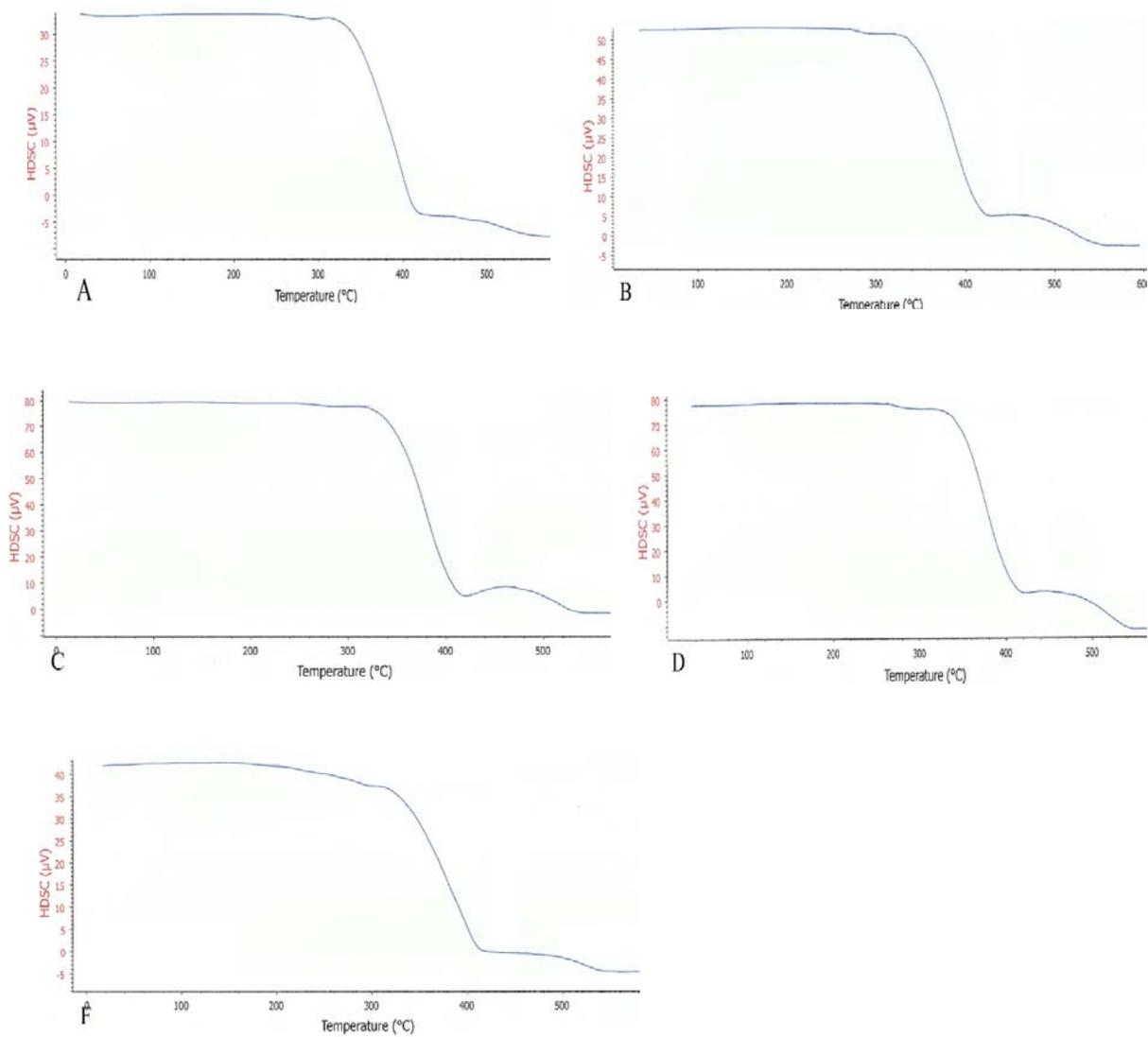


Figure (4): Thermal conductivity properties strength of blended nanocomposites versus epoxy concentration



**Figure (5):** TGA of UPR and blended nanocomposites, A:UPR, B:blend 1,C: blend<sub>2</sub>, D: blend 3, E:blend 4,F: blend 8.

## قوة انهيار العزل الكهربائي والتوصيل الحراري لمختلف السبائك النانوية المتراكبة لراتنج الايبوكسي الجديد

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### الخلاصة

يكشف هذا البحث عن تحضير وتطوير عشرة مخاليط متراكبة ومليئة بجسيمات نانوية وهي ثاني أوكسيد التيتانيوم ( $TiO_2$ ). تم تحضير شبكات البوليمر المتراكبة النانوية على أساس راتنج البوليستر غير المشبعة (UPR) وراتنجات ايبوكسي جديدة مختلفه عن طريق مزج فعال. أذ تم اختيار النسب المثلى من الجسيمات النانوية لثاني أوكسيد التيتانيوم (3%) وهي نسبة مختارة من نتائج مزجها بنسب مختلفة مع راتنج البولي استر غير مشبع. ومن ثم مزجت النسبة المثلى (3%) من ( $TiO_2$ ) مع بولي استر الغير مشبع مع نسب مختلفه من مركبات الايبوكسي الجديدة 1% , 3% , 5% و 7% من وزن راتنج البولي استر غير مشبع. وتمت مقارنة خصائص قوة انهيار العزل الكهربائي والتوصيل الحراري للمترابكات النانوية المقاسة مع تلك المواد الأساس (UPR و 3%  $TiO_2$ ). تظهر الاولى قوة انهيار العزل الكهربائي اعلى في حين التوصيل الحراري هي اقل وكما تم تحضير مخاليط لاحد تراكيب الايبوكسي رقم (2) وبالنسب المذكورة نفسها (UPR و Epoxy) و مقارنتها مع مخلوط المتراكبة النانوية لوحظه ان قوة انهيار العزل الكهربائي للمخلوط المتراكبة النانوية هو الاعلى عند نسب التحميل الواطئة للإيبوكسي رزن وكما اظهرت التوصيلية الحرارية عالية مقارنة بما اظهرته مخاليط من (Epoxy/ UPR). اجري التحليل الحراري الوزني (TGA) لدراسة الخواص الحرارية للمخاليط المتراكبة النانوية .

**الكلمات المفتاحية:** السبائك النانوية المتراكبة، البولي استر الغير مشبع، قوة انهيار العزل الكهربائي، الايبوكسي رزن.